

Ultrafine titanium filaments with a high aspect ratio fabricated by the extraction from Al + Ti composite

P. Krizik^{1*}, M. Balog^{1,2}, S. Nagy¹, L. Orovcik¹, A. Siskova^{1,3}, A. Eckstein Andicsova³

¹*Institute of Materials and Machine Mechanics, Slovak Academy of Sciences,
Dubravska cesta 9, 845 13 Bratislava, Slovak Republic*

²*Centre of Excellence for Advanced Materials Application, Slovak Academy of Sciences,
Dubravska cesta 9, 845 11 Bratislava, Slovak Republic*

³*Polymer Institute, Slovak Academy of Sciences, Dubravska cesta 9, 845 41 Bratislava, Slovak Republic*

Received 27 January 2020, received in revised form 18 May 2020, accepted 3 June 2020

Abstract

Titanium filaments were prepared by the extraction of powder metallurgy fabricated aluminum + titanium composite in sodium hydroxide solution. During the hot extrusion consolidation process, ultrafine aluminum powder particles heavily deformed the titanium powder particles into the titanium filaments of high aspect ratio and micrometric size, which were homogeneously embedded and arrayed in the aluminum matrix. The microstructure and chemistry of extracted titanium filaments were characterized in detail. For the demonstration purpose, the titanium filaments were sintered into a porous material.

Key words: aluminum (Al), titanium (Ti) filaments, composite material, extraction, powder metallurgy

1. Introduction

Titanium (Ti), known for its excellent chemical resistance and biocompatibility, has been widely applied in the chemical industry, military aircraft, and biomedicine [1]. A porous Ti structure is often utilized when an enhanced permeability or a decreased Young's modulus are of interest in the application such as corrosion-resistant filters, biomedical implants, spargers, heat exchangers, gas getters, catalyze supporters, sound and energy absorbers, electromagnetic shielding, etc. [2–4]. Various Ti pore structures, including uniform, bimodal, gradient, honeycomb-like, closed, etc. can be tailored according to the specific application [5, 6]. Porous Ti materials have been fabricated using a variety of methods and approaches such as powder sintering, additive manufacturing, foaming, space holder technique, etc. [7]. Though, most of the manufacturing techniques still possess some limitations in terms of achieving fully opened porous structure, minimum pore size, density, and surface area of porous material [5]. One of the most promising groups of porous materials with high permeability and an active surface area are those produced from Ti fibers

of micrometric size. However, owing to the limitation of the wire drawing technique, the minimum diameter of available Ti fiber is typically on the level of hundred micrometers [8]. According to the available information, the finest Ti fiber is produced by TOHO Titanium Co. LTD and has a diameter of 20 μm and a length of 2.5 mm [9]. In order to enhance the properties of Ti porous materials, Ti fibers with the size on the level of micrometers are needed. However, they are not available, as an appropriate production technology is still missing at the moment. Titanium fibers of micrometric dimensions are highly required also for the preparation of various composite materials with a polymeric or metallic matrix. In the current work, a novel technology for the production of micrometric Ti filaments with high aspect ratio by the extraction of Ti from aluminum (Al) + Ti feedstock composite material is presented.

2. Experimental

Atomized Al 99.7 wt.% powder with the mean particle size (d_{50}) of 1.15 μm and hydro-dehydration

*Corresponding author: tel.: +421232401021; e-mail address: peter.krizik@savba.sk

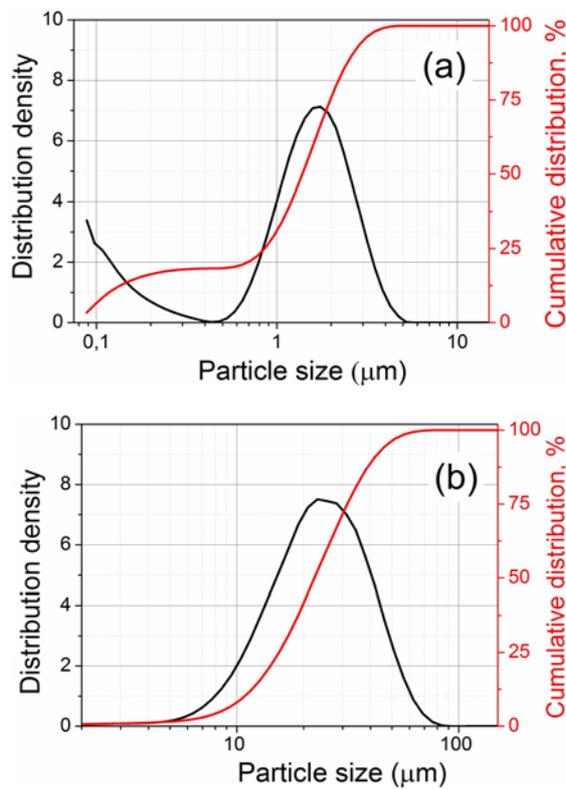


Fig. 1. The particle size distribution of used Al powder (a) and HDH Ti powder (b).

processed (HDH) Ti 99.4 wt.% powder with $d_{50} = 24.5 \mu\text{m}$ were used in this study. Particle size distribution (PSD) of used powders (Figs. 1a,b) was measured using Fritsch Analysette 22 MicroTec machine by wet dispersion in water. The chemical composition of Al powder is 0.044 wt.% silicon (Si), 0.081 wt.% iron (Fe), and bal. Al, as was determined by Inductively Coupled Plasma Mass Spectrometry (ICP-MS, ICP 5500 Perkin-Elmer). The mixture of Al + 18.52 wt.% Ti was homogenized in TURBULA shaker for 1 h. The powder mixture was precompacted by cold isostatic pressing (CIP) at 150 MPa. CIP blank was extruded into Al + 12 vol.% Ti composite rod with a diameter of 4.5 mm at the temperature of 425 °C and using the reduction ratio of 31:1, representing the true strain of 3.43. Further details on the fabrication of Al + Ti composites can be found in our previous study [10]. In order to extract Ti filaments, the extruded Al + Ti bar was dissolved in aqueous solution (10 %) of sodium hydroxide (NaOH) with 98 % purity. The filaments were purified by pure distilled water and isolated by centrifugation (Sigma 3-30K, Germany) with the rotation speed of 20 000 rpm for 10 min at 25 °C. Subsequently, the Ti filaments were dried at 45 °C for 24 h in air. To demonstrate an application of Ti filaments as a filter, the dried filaments were cold pressed at 4 MPa, and then the disk with a diameter

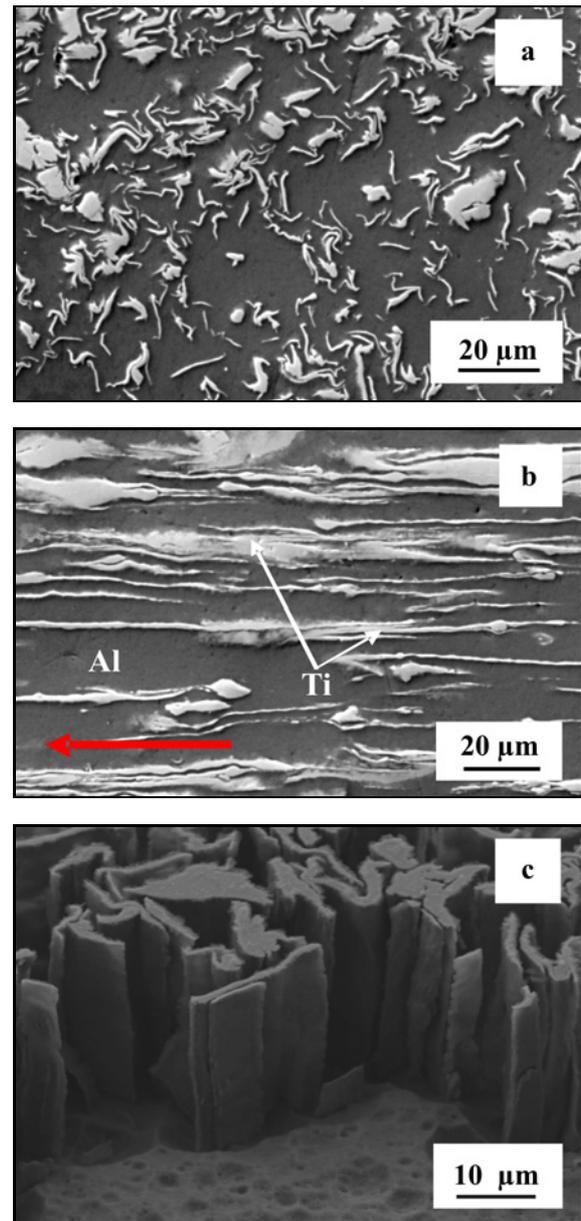


Fig. 2. SEM images of as-extruded Al + 12 vol.% Ti composite: (a) transversal, (b) longitudinal direction, and (c) deep-etched metallographic section showing the morphology of Ti filaments. (The red arrow shows the extrusion direction.)

of 5 mm and height of 2 mm was sintered at 1150 °C for 2 h in argon. The microstructure of the Al + Ti composite, the morphology of Ti powder, filaments and sintered material were characterized using scanning electron microscopy (SEM, JEOL 7500 machine) equipped with energy-dispersive X-ray spectroscopy (EDS). Interfaces between Ti filaments and Al matrix were characterized using scanning/transmission electron microscopy (STEM, FEI TITAN Themis machine) equipped with EDS. A specific surface area of

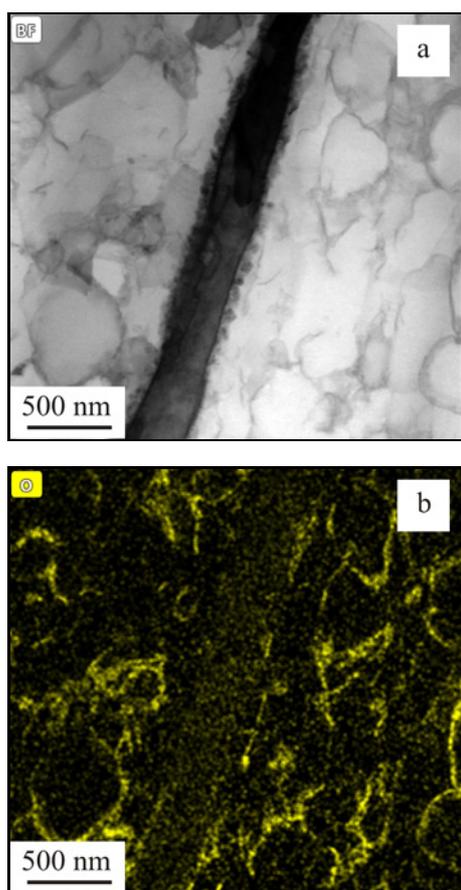


Fig. 3. Bright-field TEM image of Al + Ti composite in transversal direction (a) with the corresponding oxygen EDS map (b).

Ti powder and filaments was determined by physical adsorption (BET principle). An average thickness of filaments was calculated according to the standard stereographic intercept method [11] using SEM. The length of extracted Ti filaments was determined using SEM and was averaged over 100 measurements of individual filaments.

3. Results and discussion

The representative longitudinal and transversal cross-sections of as-extruded Al + 12 vol.% Ti composite are shown in Figs. 2a,b. High deformation resistance of fine Al powder experienced upon extrusion was comparable to the one of the coarse Ti powder. It resulted in severely textured Ti filaments elongated along the extrusion direction embedded in the Al matrix. High deformation resistance of Al powder is due to the fine Al grain size and stable nanometric network of amorphous Al_2O_3 formed at Al grain boundaries (Fig. 3), which stem from native passivation films on loose Al powder [12]. In spite of the relatively mod-

erate true strain of 3.43 induced during hot extrusion compaction step, sub-micrometric Ti filaments with an average thickness of $0.66 \pm 0.14 \mu\text{m}$ were formed. The Ti filaments exhibited a convoluted morphology as revealed by deep etching of the Al matrix in Fig. 2c. Considering the relatively low volume fraction of Ti filaments (12 vol.%), the distribution of filaments in the Al matrix is homogeneous without a notable clustering. It is a typical microstructure observed for various deformation processed metal-metal composites in the as-deformed state [13, 14]. A similar thickness of Ti filaments was also confirmed for other Al + Ti composites [15]. It is anticipated that the size, morphology, and the aspect ratio of Ti filaments could be easily adjusted by the proper selection of Al and Ti powder sizes in combination with appropriate extrusion ratio and processing temperature.

A representative interface between the Al matrix and the Ti filament is shown in Figs. 4a,b,c. In spite of the low extrusion temperature used (425°C), Al reacted with Ti during the extrusion process. For that reason, Al-Ti interfaces were enriched for Al_3Ti crystals with the size of tens of nm (Fig. 4d). Furthermore, the interface is enriched for Si, which is present as an impurity in the metallic part of Al powder and diffuses towards the Ti component. Si layer, which forms between Ti filament and Al_3Ti crystals, is amorphous with a thickness of $\sim 8 \text{ nm}$ (Fig. 4e). Owing to high deformation resistance of Al + Ti powder mixture, it was technologically not feasible using a lower extrusion temperature than 425°C , by which the formation of Al_3Ti phase and the segregation of Si could be avoided or at least suppressed. The transversal cross-section of Ti filaments is composed of a few (2–3) Ti grains with a $\langle 10\text{--}10 \rangle$ direction parallel to the extrusion direction (Fig. 4b), which is the typical texture for metals with a hexagonal close-packed structure.

Figures 5a,b compare the morphology of as-received HDH Ti powder and extracted Ti filaments. Even though some filaments fractured during the centrifugal separation, filaments with an average length of $177.3 \pm 78.5 \mu\text{m}$ were obtained by the used extraction process. This fracturing is also due to the depletion of the plasticity of Ti filaments after the extrusion process.

According to the BET analysis results, Ti filaments showed a significant increase in the value of relative surface area from 0.15 to $29.3 \text{ m}^2 \text{ g}^{-1}$ for the powder and filaments, respectively. In Fig. 6a the application of extracted Ti filaments for the fabrication of bulk porous material is demonstrated. A sound porous structure was obtained by the controlled sintering of Ti filaments, and at particular sintering conditions, the residual porosity of 42 % obtained was determined.

As measured by EDS, the sintered Ti porous sample contains 2.73 wt.% Al, 1.2 wt.% Si, and bal. Ti. Owing to the solubility of Si in Ti ($\sim 4 \text{ at.} \% \text{ Si}$ at

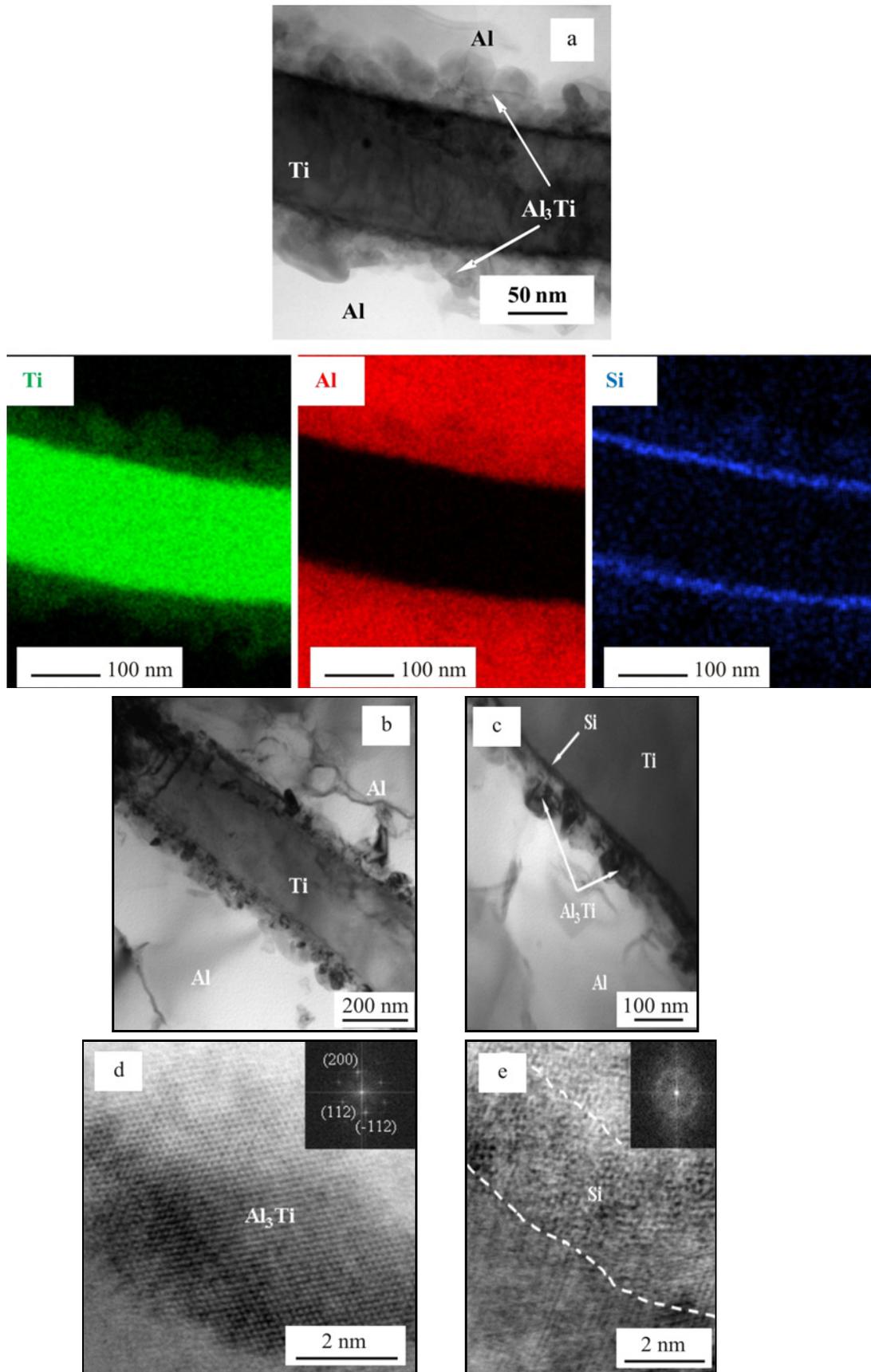


Fig. 4. (a) Bright-field STEM image of Al-Ti interface with the corresponding EDS maps of Ti, Al, and Si elements; (b, c) bright-field TEM images of Al-Ti interface; (d) bright-field HRSTEM image of Al₃Ti nanocrystal with the insert of Fast Fourier Transform (FFT) pattern of Al₃Ti; (e) bright-field HRTEM image of the amorphous Si layer with the insert of FFT pattern of Si.

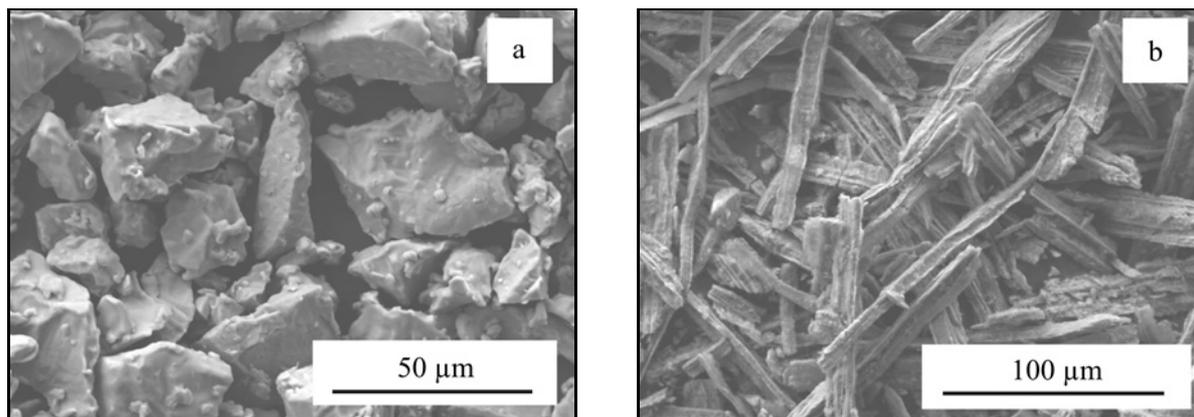


Fig. 5. SEM images of (a) Ti powder and (b) as-etched Ti filaments.

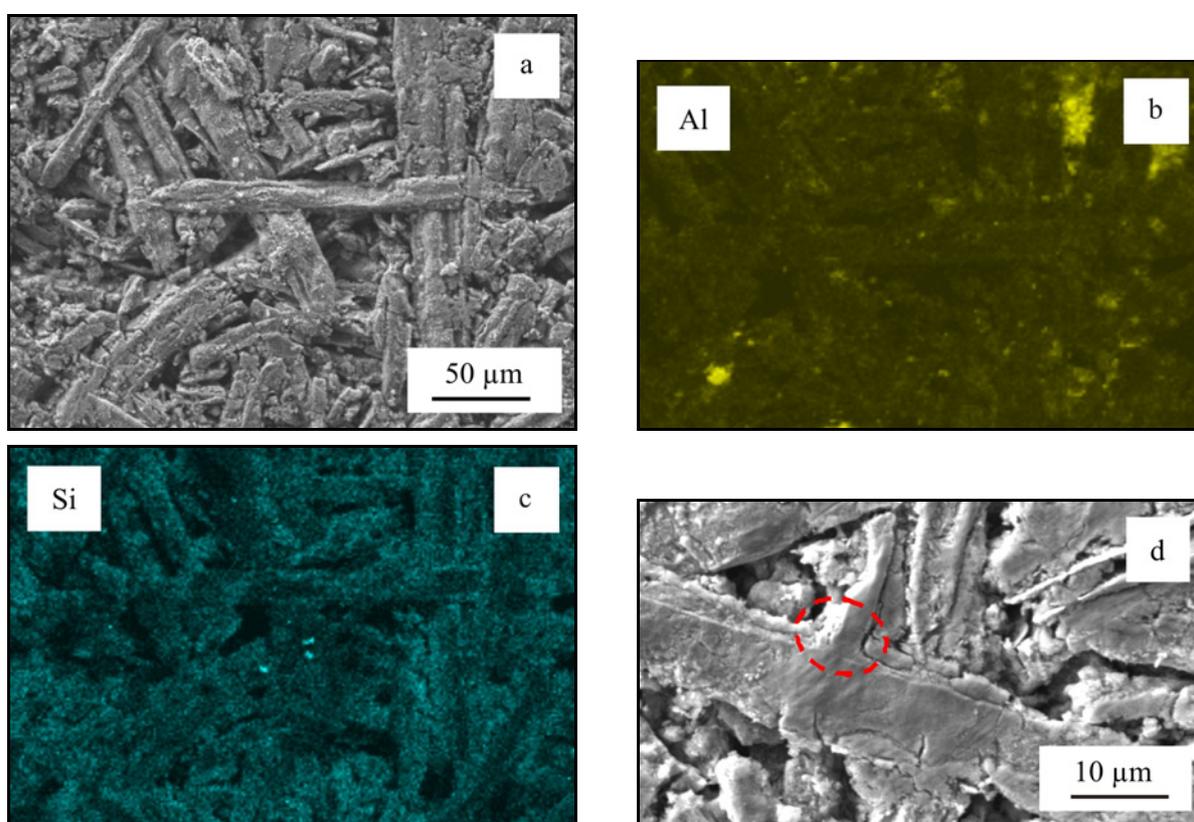


Fig. 6. SEM images of (a) the porous material sintered from Ti filaments with corresponding Al (b) and Si (c) EDS maps, and (d) the neck formed between Ti filaments during sintering (red dashed circle).

1150 °C [16]), Si atoms were homogeneously dissolved in Ti during heating up to the sintering temperature, as shown in Si EDS map (Fig. 6a). Although some areas with higher Al content were occasionally observed (Figs. 6a–c), the dissolution of Al in sintered Ti filaments can be regarded as homogeneous. For this reason, we assume that either Si or Al does not significantly influence the sinterability of Ti filaments and the properties of porous Ti material. Figure 6d shows a sintered neck formed between two adjacent Ti filaments evidencing good sinterability of extracted Ti

filaments at the used technological condition.

4. Conclusions

Ti filaments with an average thickness of 0.66 μm and with an average length of 177.3 μm were successfully synthesized by the extraction from extruded powder metallurgical Al + Ti composite in NaOH solution. The morphology, microstructure, and chemistry of extracted titanium filaments were investigated. The

extracted Ti filaments had a high relative surface area of $29.3 \text{ m}^2 \text{ g}^{-1}$. From extracted Ti filaments, a highly permeable material with resulting porosity of 42 % was prepared by the sintering.

Acknowledgements

This work was supported by the Slovak Scientific Agency under the APVV-16-0527 project, VEGA 2/0143/20 project, and VEGA 2/0114/18 project. The authors thank Mrs. V. Trembosova for help with SEM characterization. This work was performed during the implementation of the project Building-up Centre for Advanced Materials Application of the Slovak Academy of Sciences, ITMS project code 313021T081 supported by Research & Innovation Operational Programme funded by the ERDF.

References

- [1] C. Leyens, M. Peters (Eds.), Titanium and Titanium Alloys: Fundamentals and Applications, first ed., Wiley-VCH Verlag GmbH & Co. KGaA, Weinheim, 2003. ISBN: 9783527305346.
- [2] B. V. Krishna, S. Bose, A. Bandyopadhyay, Low stiffness porous Ti structures for load bearing implants, *Acta Biomater.* 3 (2007) 997–1006. [doi:10.1016/j.actbio.2007.03.008](https://doi.org/10.1016/j.actbio.2007.03.008)
- [3] Homepage GNK Powder Metallurgy, <https://www.gknpm.com/en/our-businesses/gkn-sinter-metals/porous-metal-filters/>, (accessed on January 20th, 2020).
- [4] S. F. Liu, A. Li, Y. J. Ren, D. F. Li, Z. H. Zhang, Heat transfer performance of porous titanium, *J. Iron & Steel Res. Int.* 24 (2017) 556–560. [doi:10.1016/S1006-706X\(17\)30083-3](https://doi.org/10.1016/S1006-706X(17)30083-3)
- [5] H. P. Tang, J. Wang, M. Qian, Porous titanium structures and applications. in: M. Qian and F. H. Froes (Eds.), Titanium Powder Metallurgy, Science, Technology and Applications, Butterworth-Heinemann, 2015, pp. 533–554. [doi:10.1016/B978-0-12-800054-0.00028-9](https://doi.org/10.1016/B978-0-12-800054-0.00028-9)
- [6] Z. P. Xi, J. L. Zhu, H. P. Tang, Q. B. Ao, H. Zhi, J. Y. Wang, C. Li, Progress of application researches of porous fiber metals, *Materials* 4 (2011) 816–824. [doi:10.3390/ma4040816](https://doi.org/10.3390/ma4040816)
- [7] B. Xie, Y. Z. Fan, T. Z. Mu, B. Deng, Fabrication and energy absorption properties of titanium foam with CaCl_2 as a space holder, *Mater. Sci. Eng. A* 708 (2017) 419–423. [doi:10.1016/j.msea.2017.09.123](https://doi.org/10.1016/j.msea.2017.09.123)
- [8] S. F. Liu, Z. P. Xi, H. P. Tang, X. Yang, Z. H. Zhang, Compressive behavior of porous titanium fiber materials, *J. Iron & Steel Res. Int.* 21 (2014) 793–796. [doi:10.1016/S1006-706X\(14\)60143-6](https://doi.org/10.1016/S1006-706X(14)60143-6)
- [9] Homepage TOHO TITANIUM CO. LTD., <https://www.toho-titanium.co.jp/en/products/webtjhp.html>, (accessed on January 20th, 2020).
- [10] P. Krizik, M. Balog, M. Nosko, M. V. C. Riglos, J. Dvorak, O. Bajana, Ultrafine-grained Al composites reinforced with in-situ Al_3Ti filaments, *Mater. Sci. Eng. A* 657 (2016) 6–14. [doi:10.1016/j.msea.2016.01.047](https://doi.org/10.1016/j.msea.2016.01.047)
- [11] E. E. Underwood, Quantitative Stereology, first ed., Addison-Wesley, Kittery, 1970. ISBN-10: 0201076500.
- [12] M. Balog, T. Hu, P. Krizik, M. V. C. Riglos, B. D. Saller, H. Yang, J. M. Schoenung, E. J. Lavernia, On the thermal stability of ultrafine-grained Al stabilized by in-situ amorphous Al_2O_3 network, *Mater. Sci. Eng. A* 648 (2015) 61–71. [doi:10.1016/j.msea.2015.09.037](https://doi.org/10.1016/j.msea.2015.09.037)
- [13] G. X. Wang, M. Dahms, G. Leitner, S. Schultrich, Titanium aluminides from cold-extruded elemental powders with Al-contents of 25–75 at.% Al, *J. Mater. Sci.* 29 (1994) 1847–1853. [doi:10.1007/BF00351304](https://doi.org/10.1007/BF00351304)
- [14] P. B. Wheelock, K. Wongpreedee, A. M. Russell, L. S. Chumbley, A deformation processed β -Ti + Y metal-metal composite, *J. Mater. Sci.* 37 (2002) 4307–4313. [doi:10.1023/A:1020644317324](https://doi.org/10.1023/A:1020644317324)
- [15] A. M. Russell, T. Lund, L. S. Chumbley, F. A. Laabs, L. L. Keehner, J. L. Haringa, A high-strength, high-conductivity Al-Ti deformation processed metal-metal matrix composite, *Composites: Part A* 30 (1999) 239–247. [doi:10.1016/S1359-835X\(98\)00163-8](https://doi.org/10.1016/S1359-835X(98)00163-8)
- [16] H. Okamoto, Phase Diagrams for Binary Alloys, second ed., ASM International, Ohio, 2010. ISBN-13: 978-1-61503-046-0.